

Fig. 2 $(\beta^G)^2 / \beta^G - 1$ coefficient

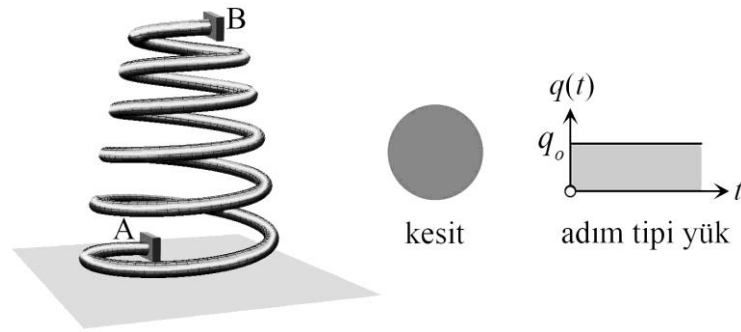
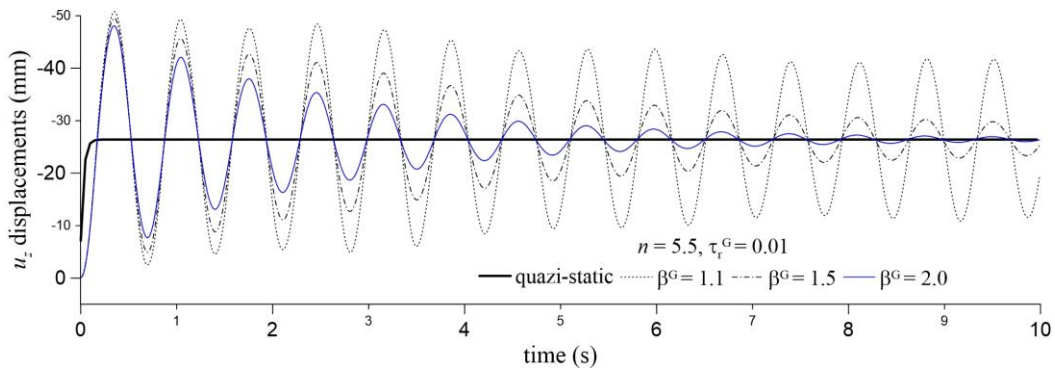


Fig. 3 The conical helicoidal rod having circular cross-section.

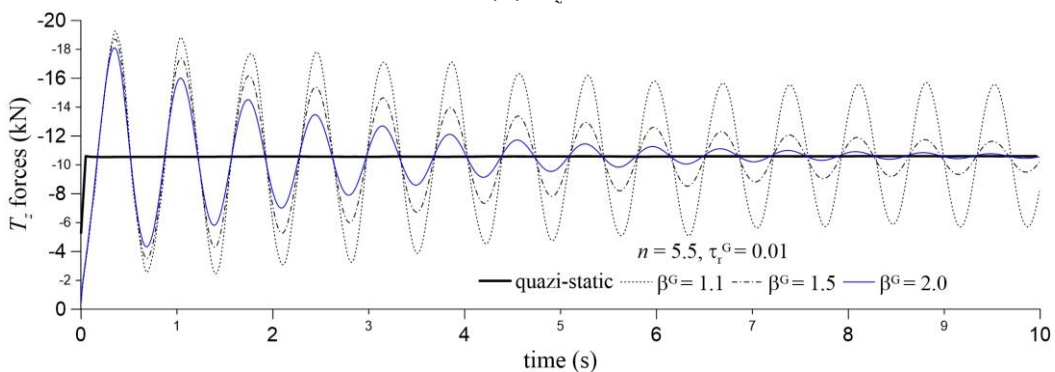
3. NUMERICAL EXAMPLES

A viscoelastic conical helicoidal rod with fixed-fixed boundary condition is solved (see Fig. 3). The helix geometry has $n = 5.5$ number of active turns, the height of the rod is $H = 5\text{m}$ and the minimum radius of helix to maximum of helix ratios $R_{\min} / R_{\max} = 0.5$ where $R_{\max} = 2\text{m}$. The circular cross-sectional diameter of the rod is $D = 20\text{cm}$. The viscoelastic material exhibits the standard type of distortional behavior while having elastic Poisson's ratio $\bar{\nu} = \nu = 0.3$. The material parameters are $G = 80\text{GPa}$, $\tau_r^G = 0.01\text{s}$, $\beta^G = 1.1, 1.5, 2.0, 3.0, 11.0$ and the density of material $\rho = 7850\text{kg/m}^3$. The form of the complex shear modulus can be obtained by using Eq. (3). The rod is subjected to a dynamic rectangular impulsive type of uniformly distributed load $q = q_z(t)$, where $q_0 = 500\text{N/m}$ (see Fig. 3). The quasi-static and dynamic responses of the rod are determined within $0 \leq t \leq 10\text{s}$. The analyses are carried out in the Laplace space and the results are transformed back to the time space numerically by modified Durbin's algorithms (Dubner and Abate 1968, Durbin 1974, Narayanan 1980). The parameters which are used in the analysis for inverse Laplace transformation algorithm are $N = 2^{11}$ and $aT = 6$ which are verified by Eratlı et al. (2014).

The vertical displacements u_z at the middle point of the helicoidal rod, the force T_z the moments M_y at the clamped end A (see Fig. 1) are determined using 100 finite elements through the analysis. The time variation curves of u_z , T_z , and M_y are depicted for $\beta^G = 1.1, 1.5, 2.0$ and $\beta^G = 2.0, 3.0, 11.0$ ratios in Figs. 4-5, respectively. The aim of these figures is to investigate the influence of viscoelastic material parameter β^G on the dynamic response of viscoelastic conical helicoidal rod. For the same values of τ_r^G retardation time, viscosity parameter η^G , and shear modulus G , there exist two different β^G ratios, except $\beta^G = 2$ that is a transition value ($G_1 = G_2$). One of these β^G ratios is between $1 < \beta^G < 2$ ($G_1 < G_2$) and the another one is $\beta^G > 2$ ($G_1 > G_2$) (see Fig. 2). G_1, G_2 values are related to viscosity part and elastic part of the standard model type viscoelastic material. In Figs. 4-5, the dashed, the dot and the solid lines are used for $\beta^G = 1.5, 3.0$, $\beta^G = 1.1, 11.0$ and $\beta^G = 2$ ratios, respectively. The responses curves of $\beta^G = 2$ values is lowest contour $\beta^G = 1.1, 1.5$ (see Fig. 4), whereas is highest contour $\beta^G = 3.0, 11.0$ (see Fig. 5). The amplitudes of u_z , T_z , and M_y (see Figs.4-5) decrease with the increasing β^G ratios, and approach to the quasi static case. When the amplitude of curves are compared Fig. 5 with respect to Fig. 4, it is observed that the amplitudes for $\beta^G > 2$ values dissipate more rapidly.



(a) u_z



(b) T_z

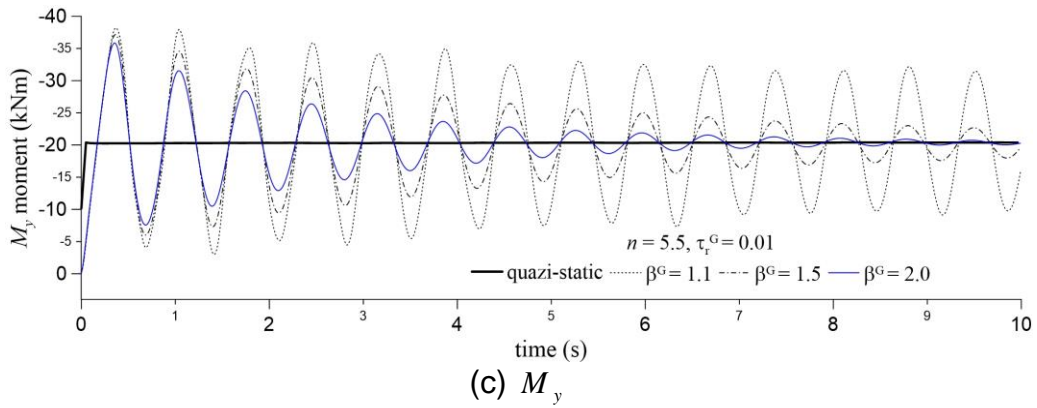


Fig. 4 Time histories of viscoelastic conical helicoidal rod for $\beta^G = 1.1, 1.5, 2.0$

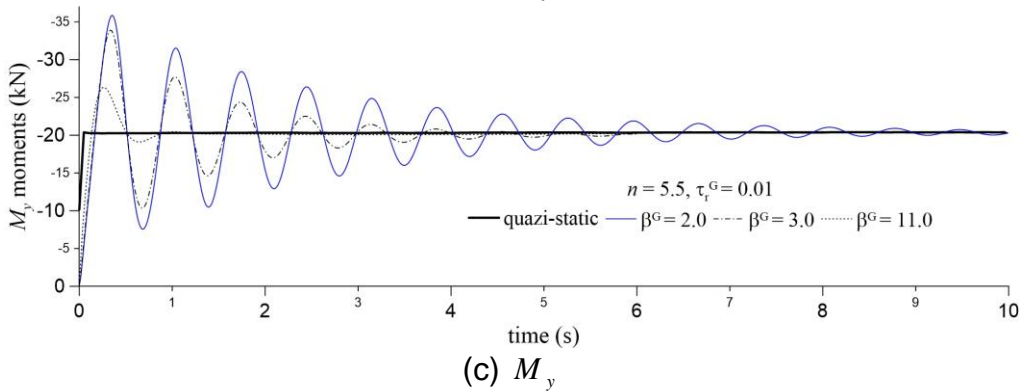
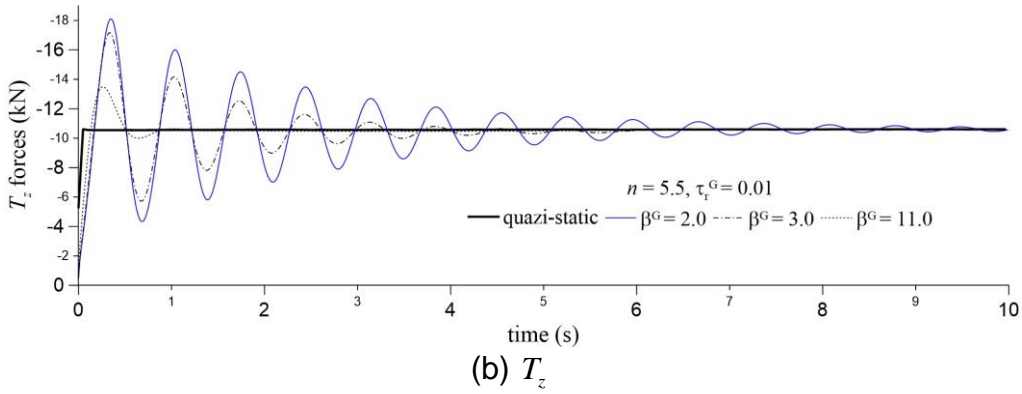
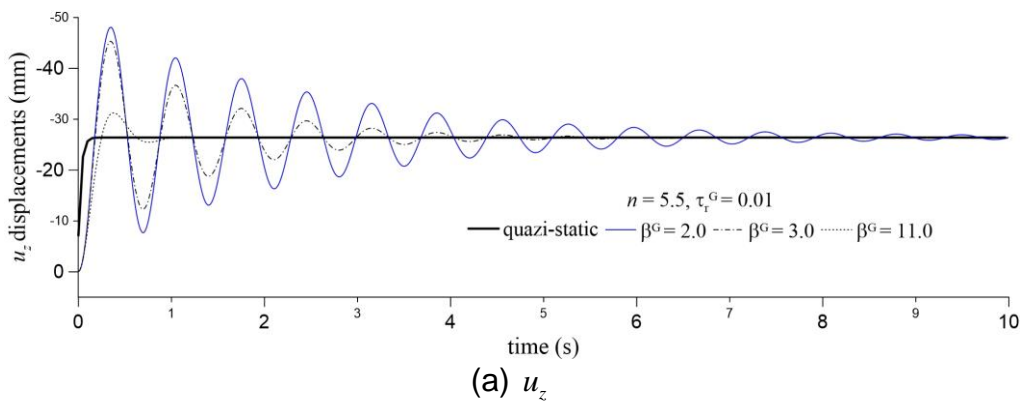


Fig. 5 Time histories of viscoelastic conical helicoidal rod for $\beta^G = 2.0, 3.0, 11.0$

4. CONCLUSION

The dynamic viscoelastic behavior under the step type of uniformly distributed dynamic load of conical helicoidal rod is examined for different viscosity parameter β^G ratio via the mixed finite element method. For this purpose, the viscoelastic material behavior is simulated by using the standard model while having elastic Poisson's ratio and the viscoelastic properties are accounted using the correspondence principle. The finite element solutions are carried out in the Laplace space. The results obtained in the Laplace space are transformed back to time space via modified Durbin's algorithm. The effects of the viscoelastic material parameter β^G ratios on the dynamic behavior of the conical helix are discussed extensively.

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REFERENCES

- Baranoglu, B. and Mengi, Y. (2006), "The use of dual reciprocity boundary element method in coupled thermoviscoelasticity", *Comput. Methods Appl. Mech. Eng.*, **196**, 379-392.
- Bortot, E., Denzer, R., Menzel, and., Gei, M. (2016) "Analysis of viscoelastic soft dielectric elastomer generators operating in an electrical circuit", *Int. J. Solids Struct.* **78-79**, 205-215.
- Chen, T. (1995), "The hybrid Laplace transform/finite element method applied to the quasi-static and dynamic analysis of viscoelastic Timoshenko beams", *Int. J. Numer. Methods Eng.* **38**, 509-522.
- Chen, W.H. and Lin, T.C. (1982), "Dynamic analysis of viscoelastic structure using incremental finite element method", *Eng. Struct.*, **4**, 271-276.
- Christensen, P.M. (1982), "*Theory of Viscoelasticity: An Introduction*", 2nd edition, Academic Press, New York.
- Dubner, H. and Abate, J. (1968), "Numerical inversion of Laplace transforms by relating them to the finite Fourier cosine transform", *J. ACM.*, **15**, 115-123.
- Durbin, F. (1974), "Numerical inversion of Laplace transforms: an efficient improvement to Dubner and Abate's method", *Comput. J.*, **17**, 371-376.
- Eratlı, N., Argeso, H., Çalım, F.F., Temel, B. and Omurtag, M.H. (2014), "Dynamic analysis of linear viscoelastic cylindrical and conical helicoidal rods using the mixed FEM", *J. Sound Vib.*, **333**, 3671-3690.
- Ermis., M. (2015), "*The dynamic analysis of non-cylindrical viscoelastic helical bars using mixed finite element method*", *MSc Thesis*, Istanbul Technical University, Istanbul.

- Ermis, M., Eratlı, N., Argeso, H, Kutlu. A. and Omurtag, M.H. (2016), "Parametric Analysis of Viscoelastic Hyperboloidal Helical Rod", *Adv. Struct. Eng.*, doi: 10.1177/1369433216643584
- Flügge, W. (1975), "*Viscoelasticity*", 2nd edition, Springer, Berlin; New York.
- Fung, Y.C. (1965), "*Foundations of Solid Mechanics*", Prentice-Hall, Englewood Cliffs, New Jersey.
- Kocatürk, T. and Şimşek, M. (2006a), "Dynamic analysis of eccentrically prestressed viscoelastic Timoshenko beams under a moving harmonic load", *Comput. Struct.*, **84** (31-32), 2113–2127.
- Kocatürk, T. and Şimşek, M. (2006b), "Vibration of viscoelastic beams subjected to an eccentric compressive force and a concentrated moving harmonic force", *J. Sound Vib.*, **291**(1-2), 302–322.
- Lewandowski, R. and Lasecka-Plura, M. (2016) "Design sensitivity analysis of structures with viscoelastic dampers", *Comput. Struct.* **164**, 95-107.
- Martin, O., A modified variational iteration method for the analysis of viscoelastic beams, *Appl. Math. Model.* (2016), <http://dx.doi.org/10.1016/j.apm.2016.04.011>
- Mengi, Y. and Argeso, H. (2006), "A unified approach for the formulation of interaction problems by the boundary element method", *Int. J. Numer. Meth. Eng.*, **66**, 816-842.
- Narayanan, G.V. (1980), "*Numerical Operational Methods in Structural Dynamics*", PhD Thesis, University of Minnesota.
- Payette, G.S. and Reddy, J.N. (2010), "Nonlinear quasi-static finite element formulations for viscoelastic Euler-Bernoulli and Timoshenko beams", *Int. J. Numer. Method Biomed. Eng.*, **26**, 1736–1755.
- Shames, I.R. and Cozarelli, F.A. (1997), "*Elastic and Inelastic Stress Analysis*", CRC Press Inc. United States.
- Temel, B. (2004), "Transient analysis of viscoelastic helical rods subject to time-dependent loads", *Int. J. Solids Struct.* **41**, 1605–1624.
- Temel, B., Çalım, F.F. and Tütüncü, N. (2004), "Quasi-static and dynamic response of viscoelastic helical rods", *J. Sound Vib.* **271**, 921–935.
- Wang, C.M., Yang, T.Q. and Lam, K.Y. (1997), "Viscoelastic Timoshenko beam solutions form Euler-Bernoulli solutions", *J. Eng. Mech.- ASCE*, **123**, 746–748.