

hysteresis loops can be compared with pushover analysis results to examine the seismic performance of the frame structure.

2. TEST SPECIMEN AND METHOD

2.1 Test specimen

A precast concrete test specimen was designed following ACI 352R-02, even though the specimen had 100% pure dry connection without the use of monolithic connection. Only the gap between the column and beam was grout-filled after the steel connector was inserted into the socket embedded in the column and fastened. A design objective was to induce plastic hinge in beam-column joints and at column-base so that a strong column-weak beam concept was applied by adjusting the relation between the column nominal moment capacity and beam nominal moment capacity. The full scale specimen is illustrated in Figs. 1(a) to 1(c).

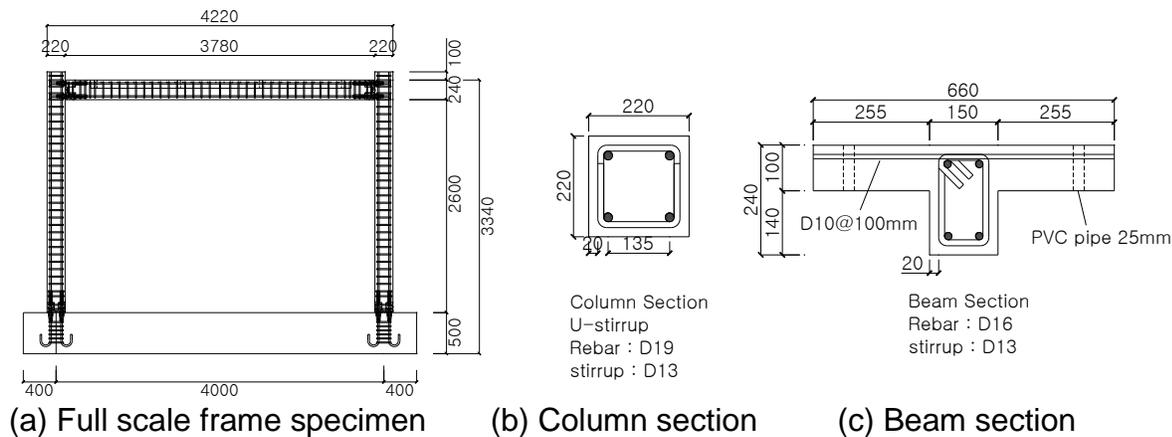


Fig. 1 Specimen details

2.2 Test method

An input earthquake ground motion was a 1999 Chi-Chi Earthquake record as shown in Fig. 2, where peak ground acceleration (PGA) was 0.79g. Deformation and acceleration of the specimen was measured by linear variable displacement transducers (LVDTs) and accelerometers, respectively.

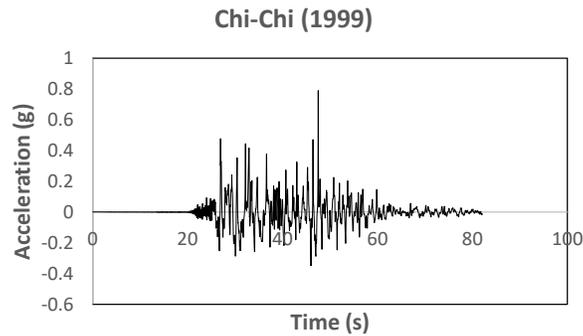


Fig. 2 Ground motion of 1999 Chi-Chi Earthquake

3. TEST RESULT AND PUSHOVER ANALYSIS RESULT

3.1 Test result

Fig. 3 represents load-deformation hysteresis loops of the specimen after the experiment was conducted. In the positive direction (right direction), at maximum load of 49.95 kN, drift ratio was 2.53%. Conversely, in the negative direction (left direction), at maximum load of 53.94 kN, drift ratio was 2.75%.

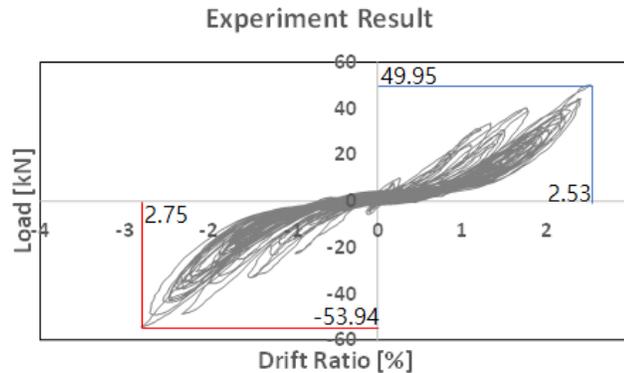


Fig. 3 Experiment result

3.2 Pushover analysis result

Pushover analysis was performed using Midas Gen program. Four hinges were defined at joints (column-base & beam-column connections). The push-over analysis result is shown in Fig. 4.

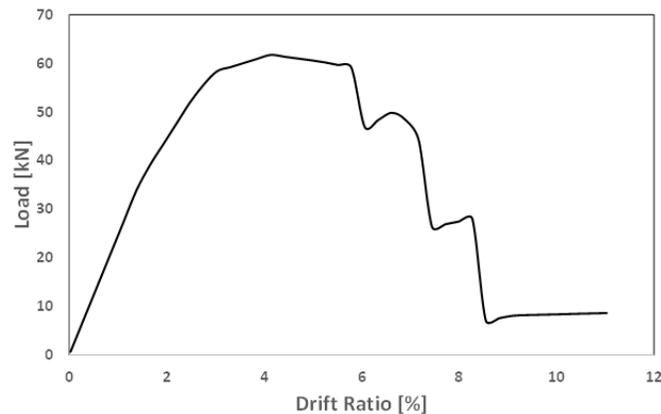


Fig. 4 Pushover analysis result

Fig. 4 shows that plastic hinges occurred at 3 points and subsequently the slope dramatically decreased. Each of the hinges failed at a load of 59 kN, 44 kN, and 28 kN, respectively, and the drift ratio at the moment was 5.8%, 7.2%, and 8.3%.

3.3 Comparison of experiment and pushover analysis results

Comparison of experiment and pushover analysis results is made in Fig. 5. By comparing the experimental result and pushover analysis result, the dynamic performance level of the specimen was found to be similar to the quasi-static performance level at least up to 2.75% drift level. This indicates that the frame behaved just like an RC frame with monolithic connection, as the modeling was done assuming the rigid RC connection.

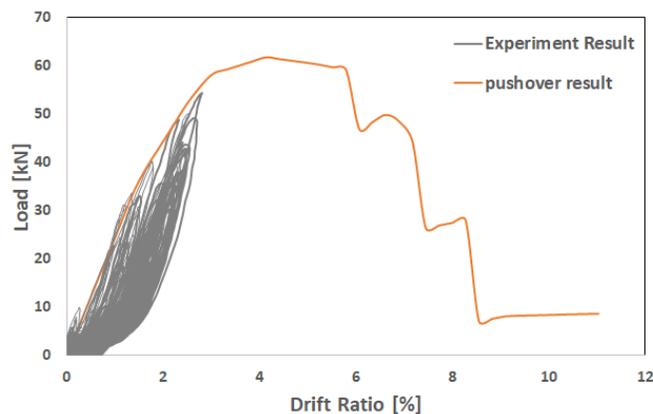


Fig. 5 Experiment and pushover analysis results

3. CONCLUSIONS

*The 2020 World Congress on
The 2020 Structures Congress (Structures20)
25-28, August, 2020, GECE, Seoul, Korea*

A precast concrete frame structure with pure dry connection was tested on the shaking table in one-axis direction. A 1999 Chi-Chi Earthquake ground motion was applied, and the damage on the structure developed according to the intensity of earthquake ground motion was observed. The structure experienced the elastic and plastic stages of deformations without a loss of capacity or collapse. For further research on the behavior of the precast frame structure, a pushover analysis was conducted. From the studies, the following conclusions can be drawn:

- (1) The precast concrete frame structure endured a 1999 Chi-Chi earthquake without a loss of lateral load carrying capacity or collapse, and maintained stable ductile behavior until the end of one-axis shaking with PGA of 0.79g. The drift ratio of the structure of up to 2.75% was recorded, which occurred at the maximum load. This is above the allowable maximum drift ratio (1.5%) of a frame structure that should retain sufficient seismic capacity.
- (2) The pushover analysis result shows that the structure's performance is similar to the quasi-static performance of a rigid moment frame up to 2.75% drift level.
- (3) Further research would be needed on the plastic motion, energy dissipation ability and reduction of structure stiffness according to the degree of cracks.

REFERENCES

- ACI Committee 352 (2002), "Recommendations for Design of Beam-Column Connections in Monolithic Reinforce Concrete Structures (ACI 352R-02)", *American Concrete Institute*.
- KCI (2012), "Concrete Design Code and Commentary", *Korea Concrete Institute* (in Korean).
- Li, S., Zuo, Z., Zhai, C., and Xie, L. (2017), "Comparison of Static Pushover and Dynamic Analyses Using RC Building Shaking Table Experiment", *Engineering Structures*, 136, 430-440.